

## Photovoltaic System under Uneven Light Condition and Variable Load with Modified Incremental Resistance Algorithm

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**Key words:** Local MPPTs, Global MPPTs, MPPTs, Uneven Lighting Conditions (ULCs), Incremental Resistance (INR)

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**Abstract:** On scrutinizing P vs. V curves of P\_V arrays which receives non\_uniform insolation of light or simply during Uneven\_Lighting\_Conditions (ULCs) multiple LMPPTs are exhibited. Conventional MPPT methods are efficient in normal conditions even though they failed to identify the GMPPTs from LMPPTs under ULCs. To improve productivity of Maximum\_PPT method for P\_V arrays under both ULCs and normal conditions some modifications are tried in this study. The Incremental\_resistance\_method added with some alterations enables to track the LMPPTs as well as GMPPTs very effectively and accurately with less numbers of steps. In proposed system, losses during GMPP tracking is minimized under ULCs. Simulation is performed in MAT\_LAB.

## INTRODUCTION

Surmount the paucity of energy, Sun is the effective option. But the incipient expenditure and the vast land requirement made the choice impediment. So, an infinitesimal loses in power results unprofitable. If wisely used this energy could overcome energy demands and moreover it is clean and easily available.

Global-MPPT of P\_V array in all conditions guarantee the extreme power possibly obtained from sun. Popular MPPT methods like ripple correlation technique, Short\_Circuit\_Current (SCC) technique and Incremental\_Conductance (IC) methods are effective during normal light insolation condition but these methods seems to be struggled to find GMPPTs under ULCs conditions, i.e., when modules of solar array didn't receives uniform insolation of light. During normal solar insolation conditions P vs. V curves of PV arrays exhibit only one peak, Multiple LMPPTs may be viewed in P vs. V curves of P\_V arrays under ULCs. Hence, several

MPPT methods are proposed, especially, applicable for solar arrays under ULCs which can be listed into two groups: hardware\_based and software\_based methods.

By Hsieh *et al.*<sup>[1]</sup> INC-algorithm is modified to solve a simple first degree polynomial equation to locate Global-MPP but hardware Complexity is being increased as it require more measuring components and circuits also it couldn't assure to locate Global-MMP in P Vs V curves which is having more number of peaks.

By Femia *et al.*<sup>[2]</sup> P&O algorithm, is modified by adjusting he duty cycle between maximum and minimum value of dc/dc\_converter and almost all the LMPPs are identified but consumption of time is more. By Kollimalla and Mishra<sup>[3]</sup>. Fuzzy\_logic based HC algorithm stores all the inter maximum values repeats in MCU and from saved data Global-MPPT is obtained using fuzzy. Although, the system become precise one but complexity of system and time consumption increased, consequently it get less importance.

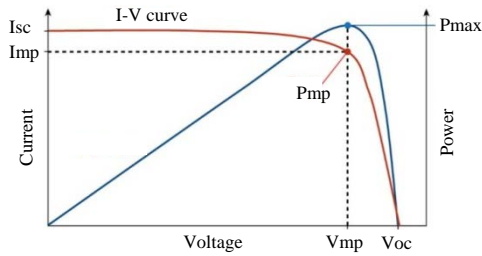


Fig. 1: P\_V and IV characteristics of P\_V module under normal light condition

By Liu *et al.*<sup>[4]</sup> particle\_swarm\_optimization GMPPT is located precisely using a velocity equation, even though error in setting governing equation parameters may cause entire system disrupt. Figure 1 shows the Pow-Volt and I(current)-Volt characteristics of P\_V module during normal light condition.

An extensive research on P\_V curves under ULCs reported by Ramyar *et al.*<sup>[5]</sup> reveals the hike in the curve occurs approx at the  $0.8 \cdot V_{oc}$  and curve exhibit the tendency to rise before GMPP and fall afterwards considering above characteristics PO- algorithm is mostly utilized to identify the LMPPs and Global-MPP<sup>[5]</sup>. Even though under ULCs the accuracy of P\_O algorithm is doubtful.

Here, a method which finds GMMP under ULCs very accurately along with good performance in above mentioned factors is tried. This system perform by mapping solar insolation pattern using the P\_V current measured at defined points and choose appropriate points for LMPPT, then it performs INR in these points and all the LMPs are obtained by LMPs comparison GMP is identified.

## MATERIALS AND METHODS

**Proposed algorithm:** In this, a few conclusion under ULCs reported by Ramyar *et al.*<sup>[5]</sup> are employed. The conclusion referred are the hike in curve occur approx. at the  $0.8V_{oc}$  and curve exhibit the tendency to rise before GMPP and fall afterwards. Here, Incremental\_resistance is realized instead of P\_O because of its consistency under ULCs. A new algorithm is introduced to track the MPPs instantly. From above conclusion, the GMPP may be located in the middle of three successive hikes or it may be situated at either ends of the Power-Volt curve. Consequently, there exist 3 types of hike in Pow-Volt\_curve (Fig. 2).

The 1st one is where the Global-MPP lies in mid of the others LMPPs as in Fig. 2. The other 2 probability are the location of the Global-MPP at the either side of the Pow-Volt\_curve and the value falls when hikes are far away from the Global-MPP, refer curve 2 and 3 in Fig. 2. In all these Local-MPPs, the proposed set of rules NDS

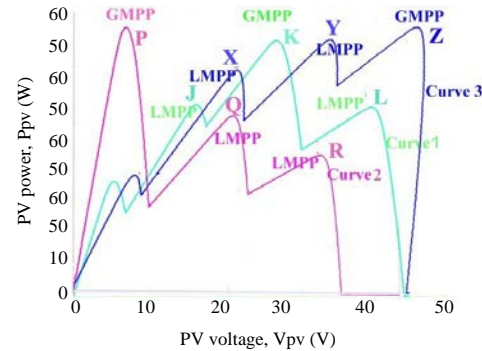


Fig. 2: Pow-Volt curves of the P\_V array under ULCs

three successive hikes and identify the highest value. If Global-MPP is not available in the mid of the 3 hikes, the algorithm advances to exploit until the Global-MPP is in the mid or until the end of the Pow-Volt curve where the min or max achievable voltage is showed up. Following sections dealt with the set of rules used to record the Global-MPP in 3 distinct types of multiple hikes Pow-Volt curve. The two variables taken are the  $V_{oc}$  of the P\_V module and the max number of series-connected module (Mmax).

**Case I; Global-MPP lies in the middle of other two local-MPPs:** Refer to flowchart, Fig. 3 initially, the values of power  $P_{mpp\_1}$ ,  $P_{mpp\_2}$ ,  $P_{mpp\_3}$  and duty\_cycles  $Duty\_1$   $Duty\_2$   $Duty\_3$  are adjusted to zero value (block\_1). Then Mmax and the  $V_{oc}$  are adjusted (block\_2). Afterwards the conventional INR method (block\_3) is utilized to get maximum\_power at point\_J (curve1) see Fig. 2, then converter's duty\_cycle is saved into  $Duty\_1$  and the power is saved into  $P_{mpp\_1}$  (block\_4). Afterwards check whether  $V_{max}$  ( $V_{oc}$  multiplied with Mmax) is attained or not (block\_5), if not attained the algorithm will search right side of point\_J to get new MPP (curve 1). As in [13] at MPPs the value of voltages vary with  $0.8 \cdot V_{oc}$  from each other therefore  $V_{ref}$  is incremented by  $0.8 \cdot V_{oc}$  to  $V_{mpp\_1}$  (block\_6).

Then to ensure convergence of point of operation of the P\_V array very close to point\_K a subroutine MPP tracker (block\_7) is used in Fig. 3 before the INR method (block\_8) is utilized to identify the maximum\_power at point\_K. Consequently at point\_K converter's duty\_cycle is stored as  $Duty\_2$  and power is stored as  $P_{mpp\_2}$  (block\_9). If  $P_{mpp\_2}$  value at point\_K is higher than the value of  $P_{mpp\_1}$  (block\_10) see Fig. 3 the algorithm moves to block\_11 and  $P_{mpp\_1}$  and  $Duty\_1$  at point\_J is replaced with  $P_{mpp\_3}$  and  $Duty\_3$ . Then,  $P_{mpp\_2}$  and  $Duty\_2$  point\_K are saved into  $P_{mpp\_1}$  and  $Duty\_1$ . In brief  $P_{mpp\_1}$  always contains highest value of MPP. Then it goes back to block\_5 and continues the search to identify  $P_{mpp\_2}$  at right side of  $P_{mpp\_1}$  from block 6 to block\_9 until the  $V_{max}$  is reached.

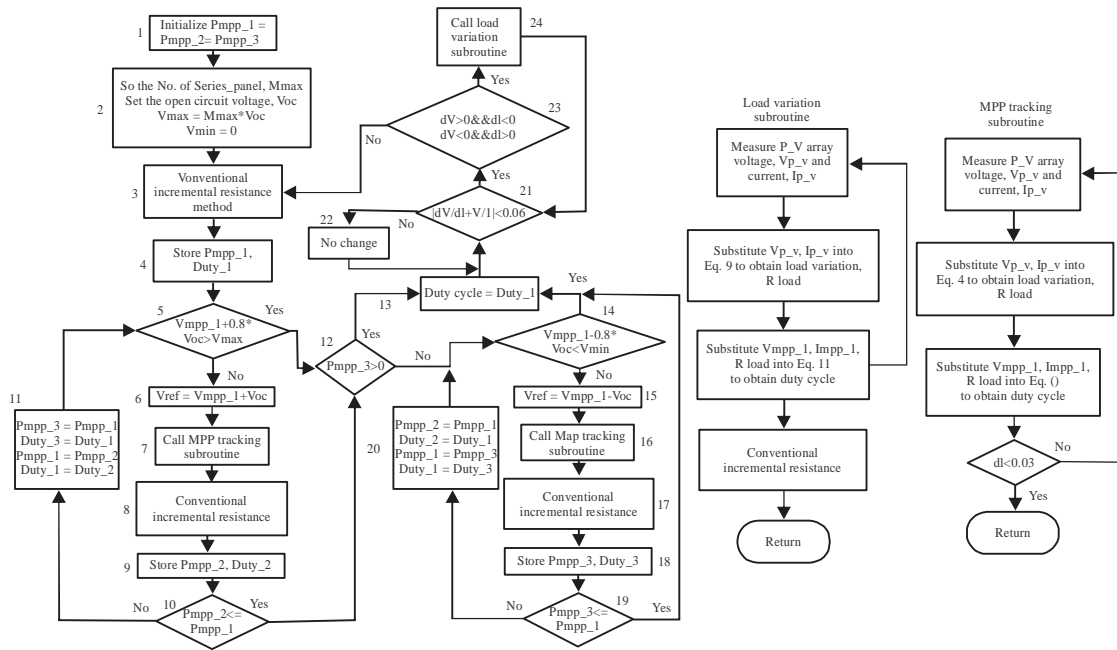


Fig. 3: Flowchart of proposed system

Algorithm reach block\_12 when the value of Pmpp\_2 at point\_L is below Pmpp\_1 at point\_K .Since Pmpp\_3 has data of point\_J, Duty\_1 will be used as the dc/dc\_converter's on-off period (block\_13) after that returns to block\_21. To ensure P\_V system is still at GMPP equation\_1 is utilized:

$$\frac{dV}{dI} + \frac{V}{I} \leq 0.06 \quad (1)$$

Generally, Eq. 1 is equates to zero but in real situation it is not possible to get zero because of truncation\_error, hence, 0.06 error is permitted to terminate the fluctuations while operating under steady-state and thereby, increasing the P\_V system efficiency. Then, it goes from block\_21 to block\_22 and then back to block\_21 as long as there is no ULCs.

Afterwards, the algorithm moves to block\_23 and changes in voltage as well as current is identified. The transition in current as well as voltage of the P\_V array during ULCs is referred in Table 1. When load resistance changes the voltage variation will be different from current variation. Hence, subroutine load variation is called to ensure tracking of GMPP very quickly. If there occurs a change in solar insolation rate the changes occurs in current and voltage are similar. Then the proposed algorithm restarts from block\_3 to track maximum current and voltage of P\_V array.

**Case\_II; GMPP located left side or right side of all the MPPs:** As same as first case variables such as Voc, Mmax are set (blocks\_1 and block\_2). Then, the

Table 1: Voltage and current variation under ULCs

Parameters	Variation in current (dI)	Variation in voltage (dV)
<b>Solar insolation</b>		
Increases	Increases	Increases
Decreases	Decreases	Decreases
<b>Load resistance</b>		
Increases	Decreases	Increases
Decrease	Increases	Decreases

Increment\_resistance (block\_3) is utilized to obtain the Maximum\_power at point\_Q in curve 2 similarly it finds Point\_X in curve 3 and the P\_V array's power and on-off period of the dc/dc\_converter are stored into Pmpp\_1 and Duty\_1 (block\_4). Afterwards, it check whether Vmax (Voc multiplied with Mmax) is attained or not (block\_5), if not attained the proposed\_algorithm will search right side of point\_Q to get new MPP (block\_6 to block\_9) in case of curve 2, similarly proposed\_algorithm will search right side of point\_X to get new MPP (block\_6 to block\_9) in case of curve 3. Then in curve 2 the proposed\_algorithm compares Pmpp\_2 point\_R to Pmpp\_1 point\_Q (block\_10) and in case of curve 3 it compares Pmpp\_2 point\_X to Pmpp\_1 point\_Y (block\_10). Since, Pmpp\_2 lower than Pmpp\_1 the algorithm jump to block\_12 in case of curve 2 and jumps to block\_11 in case of curve 3. If Pmpp\_3 value is not registered yet block\_13 and the Vmin is not equal to zero (block\_14) the algorithm continues to identify Pmpp\_3 point\_P the left hand side of Pmpp\_1 in case of curve 2 and algorithm continues to identify Pmpp\_3 point\_Z the right hand side of Pmpp\_1 in case of curve 3. The Vref is decreased by 0.8\*Voc (block\_15) in case of curve 2 and

increased by  $0.8 \cdot V_{oc}$  in case of curve 3. A subroutine MPP tracker (block\_16) is call up on to obtain the point of operation of the P\_V array nearer to the maximum\_power at point\_P before the INR (block\_17) is utilized to identify the Pmax at point\_P. The value of point\_P are saved into Pmpp\_3 and Duty\_3 (block\_18). Since, Pmpp\_3 point\_P is more compared to Pmpp\_1 point\_Q, the data of point\_Q are now saved to Pmpp\_2 and Duty\_2 and the values of point\_P are now saved into Pmpp\_1 and Duty\_1 (block\_20). Then, the algorithm return to (block\_14) and Duty\_1 is used as the converter's duty\_cycle since Vmin is achieved. In the case of curve 2, the P\_V system operates at the leftmost side of the P\_V curve (point\_P) which is its Global-MPP, similarly, the P\_V system operates at the rightmost side of the P\_V curve (point\_Z) which is the Global-MPP in case of curve 3. Finally, the algorithm starts looping between block\_21 to 22, till it observe any variation in ULCs.

**Conventional increment resistance method:** Power (P) when differentiated w.r.t Current I and equate to zero variables of INR algorithm is obtained. Consequently, the slope of the P\_V array will be zero at maximum\_power Point, also negative or positive on either side of maximum\_power point, given by:

$$\begin{aligned} \frac{dP_{p-v}}{dI_{p-v}} &= 0, \text{ MPP} \\ \frac{dP_{p-v}}{dI_{p-v}} &> 0, \text{ MPP left} \end{aligned} \quad (2)$$

$$\frac{dP_{p-v}}{dI_{p-v}} < 0, \text{ MPP right}$$

Since:

$$\begin{aligned} \frac{dP_{p-v}}{dI_{p-v}} &= \frac{d(I_{p-v} V_{p-v})}{dI_{p-v}} = V_{p-v} + I_{p-v} \frac{dV_{p-v}}{dI_{p-v}} \\ &\cong V_{p-v} + I_{p-v} \frac{\Delta V_{p-v}}{\Delta I_{p-v}} \end{aligned} \quad (3)$$

Equation 3 becomes

$$\begin{aligned} \frac{\Delta V_{p-v}}{\Delta I_{p-v}} &= -\frac{V_{p-v}}{I_{p-v}}, \text{ MPP} \\ \frac{\Delta V_{p-v}}{\Delta I_{p-v}} &> -\frac{V_{p-v}}{I_{p-v}}, \text{ MPP left} \\ \frac{\Delta V_{p-v}}{\Delta I_{p-v}} &< -\frac{V_{p-v}}{I_{p-v}}, \text{ MPP right} \end{aligned}$$

The maximum\_power point can thus be identified by matching the values of  $V_{p-v}/I_{p-v}$  with the  $\Delta V_{p-v}/\Delta I_{p-v}$ . Iref is the reference\_current at which the P\_V array is pushed to operate. At the maximum\_power point, Iref

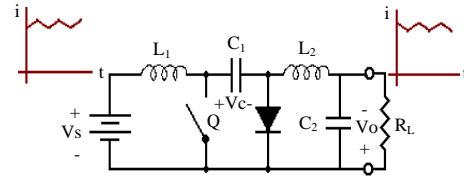


Fig. 4: Dc/Dc\_CUK converter circuit

becomes IMPP. Once the maximum-power point is achieved, the point of operation of P\_V array is maintained at that level until a variation in voltage is noted indicating ULCs. The value of Iref is decreased or increased to identify the new maximum\_power point. The P\_V array Pout is applied to directly control the dc/dc\_converter output Iref which is also the output Iref of the P\_V array, contributing to a noncomplex control-system.

**Calculate duty cycle for CUK converter:** A dc/dc-converter is connected between P\_V and load. Equation 5 and 6 show the relationships between the output-voltages and input\_current of the dc/dc\_converter (CUK). Figure 4 shows CUK converter circuit:

$$V_{in} = \frac{1-D}{D} V_{out} \quad (5)$$

$$I_{in} = \frac{D}{1-D} I_{out} \quad (6)$$

Divide Eq. 5 by Eq. 6 to get Eq. 7:

$$Z_{in} = \frac{(1-D)^2}{D^2} Z_{out} \quad (7)$$

Where:

D→converter's Duty\_cycle

$V_{in}$ →converter's input voltage

$I_{in}$ →converter's input current

$Z_{in}$ →converter's input impedance

$Z_{out}$ →converter's output impedance

$Z_{load}$ →Load impedance

In the PV system (Eq. 7) can be rewritten to obtain Eq. 8 and 9:

$$\frac{V_{p-v}}{I_{p-v}} = \frac{(1-D)^2}{D^2} Z_{load} \quad (8)$$

$$Z_{load} = \frac{D^2}{(1-D)^2} \frac{V_{p-v}}{I_{p-v}} \quad (9)$$

At any operating point ( $V_{p-v}$ ,  $I_{p-v}$ ) of the P\_V array and the D is known, the  $Z_{load}$  at the converter output can

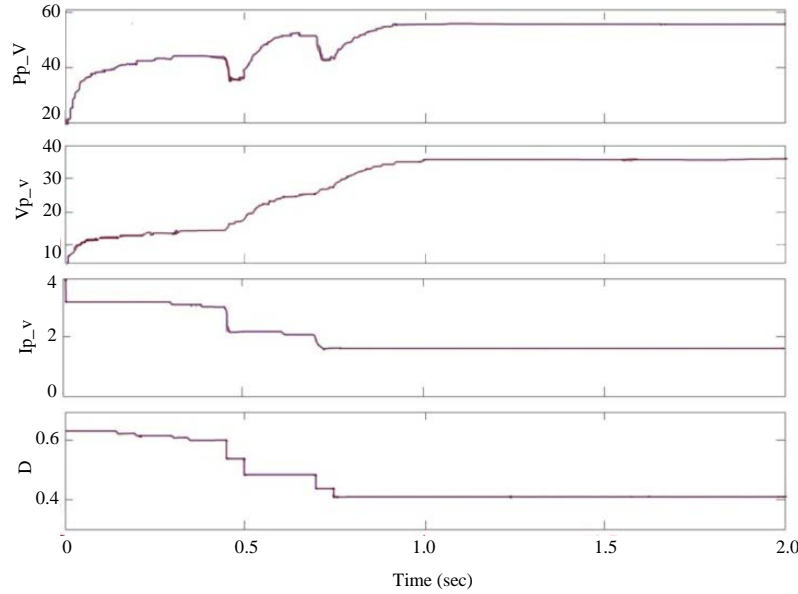


Fig. 5: Results of simulation for the P\_V system under uneven lighting conditions where the solar insolation values for each of the 18-series\_connected P\_V cells are (a) 1.2, 0.8, 0.6 and 0.5  $\text{kW}^{-2}$

be obtained by using Eq. 9. After getting the value of load impedance, Eq. 9 becomes Eq. 10. With known voltage and current of the P\_Varray, using Eq. 11 the on-off period (Duty\_cycle) can be calculated. This Duty\_cycle is utilized by converter to required voltage and current:

$$\frac{D^2}{(1-D)^2} = \frac{I_{p\_v}}{V_{p\_v}} Z_{load} \quad (10)$$

$$D = \frac{\sqrt{\frac{I_{p\_v}}{V_{p\_v}} Z_{load}}}{1 + \sqrt{\frac{I_{p\_v}}{V_{p\_v}} Z_{load}}} \quad (11)$$

## RESULTS AND DISCUSSION

The model of P\_Varray under ULCs, the CUK\_converter and Maximum-PPT controlled are generated in a MAT\_LAB Simulink model. These specifications of the P\_V module in the P\_Varray refer Table 2.

The converters component values are:  $C_{in}$  and  $C_{out} = 3900 \mu\text{F}$ ,  $L1$  and  $L2 = 125 \mu\text{H}$  and  $10\text{-}\Omega$  resistance as load. The switching frequency for the switch (Insulated-gate-bipolar-transistor) is adjusted to 25 kHz. In this, maximum power point tracker controller sampling time is adjusted to 0.05s and the converter's duty\_cycle step size is set to 0.005. Model have one by\_passdiode across eighteen-series connected P\_Vcells

Table 2: Specification of P\_V Module (KC85T) under 25°C and 1000 W insolation

Quantity	Values	Units
Maximum power	86.95	W
MPP voltage	17.44	V
MPP current	5.02	A
Voc	21.7.0	V
Isc	5.34	A
No. of series cells	36.00	
No. of series cells with Bypass diodes	18.00	

in the module which means 2 by\_passdiodes in one P\_V module. Therefore, there are maximum chances of producing 2 maximum-power points by one P\_V module during ULCs. Therefore, here, Voc is taken as 10.8V which is half times the Voc of the P\_V module. Then, parallel connected by\_passdiode P\_V module create the P\_V array. Hence, two-series connected P\_V modules have maximum of 4 hikes during ULCs. Figure 5 shows the simulation results for two different ULCs where 4 distinct level of solar insolation on each of the eighteen-series\_connected P\_V cells in the two-series\_connected P\_V modules. Initially, using conventional INR method first MPP, (P1) is identified (which is stored into Pmpp\_1) and then the algorithm goes to the right of P1 (uses MPP tracking subroutine algorithms in block\_7 for fast computation of duty\_cycle) to find the next MPP (P2). Since, P2 (51.4 W) is greater than P1 (44.1 W), the power at P1 is now stored into Pmpp\_3 and the power at P2 is stored into Pmpp\_1. Then, the algorithm goes to the right of P2 again and tracks the next MPP at P3. After that the power at P2 is stored into

Pmpp\_3 and the power at P3 is stored into Pmpp\_1 because P3 (56.4 W) is greater P2 (51.4 W). Then, the algorithm stops the searching process because Vmax (43.2V) is reached and Duty\_1 is used as the duty cycle of the converter, since, P3 has the largest power among the others and it is at the right most side of the P\_V curve. Finally, the power of P\_Varray is observed in block\_21.

### CONCLUSION

In this study, a modified incremental\_Resistance algorithm has been used to identify the Global-MPP for the P\_Varray under uneven light conditions and also load variation. To increase the response of maximum-power point identifying system a new algorithm is used in which turn on and turn off period of converter is adjusted. The simulation results shows that the Increment\_Resistance method added with some alterations enables to track the LMPPTs as well as Global MPPTs very effectively and accurately with less numbers of steps. In proposed system, losses during Global MPP tracking is minimized under ULCs.

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