

Effect of Spacing on Flow Field Characteristic of Tube Artificial Reefs with Parallel Formation by CFD

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Abstract: In addition to attracting to fish, the flow field characteristics around Artificial Reefs (ARs) are key factors to prevent beach erosion. In the present study, research on hydrodynamics of artificial reefs primarily focusing on numerical simulation is conducted. The tube artificial reefs with parallel formation is analyzed based on comprehensive three-dimensional Computational Fluid Dynamic (CFD) approach by Renormalization Group (RNG) $k-\epsilon$ turbulent model with respect to the length of slow flow region. The arrangement of artificial reefs is applied varying the spacing between the AR units both in transversal and longitudinal direction. The numerical results indicate that a greater artificial reef effect dealing with the slow flow region is obtained when the distance between the AR units of artificial reef is relatively close. According to the results, the largest slow flow region is achieved when the three rows of AR units is used. This result can be considered as a guide to reduce the beach erosion.

Key words: Abrasion, Artificial Reef (AR), Computational Fluid Dynamic (CFD), slow flow region, transversal, longitudinal

INTRODUCTION

Artificial Reefs (ARs) have been extensively used to increase total biomass production including fish when they are deployed in the sea (Bohnsack and Sutherland, 1985). Recent studies have presented the significant effect of flow fields around reefs from the perspective of ecological term and hydrodynamic term. Based on hydrodynamic point of view of the artificial reef, Ontowirjo and Armono (2003) using a numerical modeling approach observed the hydrodynamic parameters (i.e., particle velocities, fluid flows, wave breaking and dissipation of wave energy) of a, specially, shaped submerged structure to reduce the offshore waves energy as well as to provide a safe and productive environment for fish. Miao and Xie (2007) studied the effects of water-depth on the hydrodynamic force of the artificial reef by simulating regular and irregular waves. They found that in the ultra-shallow water hydrodynamic force increases very evidently with the decrease of water-depth. Jiang *et al.* (2010, 2013) developed a numerical method to investigate the hydrodynamic

characteristic of artificial reef and found that the numerical simulation results are in a good agreement with results observed by experimental means. Thus, they suggested that the numerical simulation method can be applied to predict the hydrodynamic behavior associated with artificial reefs. Other interesting result was drawn by Woo *et al.* (2014). They proposed a numerical method which can be applied to predict the drag coefficients of the artificial reefs. Later, more works have been conducted by Kim *et al.* (2014) focusing not only for drag coefficients but also for wake region and structural response of the general ARs to make more attractions to marine bio creatures and the stability in water flow.

The issue of what shape of artificial reef can affect very much the flow fields has also attracted significant attention from engineers and marine ecologists. Liu *et al.* (2012) used the numerical simulation and experiment methods to study the flow fields within and around a hollow cube artificial reef varying the sizes of hollows. Later, Liu *et al.* (2013) studied the flow field characteristics around star-shaped artificial reefs. In their research, they discussed the influence of arrangement and spacing on

the flow field of one and two artificial reefs. In recent publication, Jiao *et al.* (2017) studied the effect of flow fields around tube artificial reefs based on the numerical simulation and PIV experimental. It was found that a greater unit artificial reef effect is obtained when five reefs are involved and the ratio of reef unit height to water depth is 0.224. In addition, some researchers also showed that the flow field could be affected by the arrangement of the artificial reefs (Suzuki *et al.*, 2011; Liu and Su, 2013).

Based on literature survey mentioned, it seems that most of studies focused on the deployment of the artificial reef for coral restoration. Therefore, in the current study based on the hydrodynamic point of view, it is essential issue to investigate the flow field within and around the artificial reefs with respect to the enhancement of the artificial reefs performance for preventing beach abrasion. The main idea of this research is how the Artificial Reef (AR) arrangement could generate the longest slow flow region.

Following the main frame of this idea with respect to the flow characteristic around the Artificial Reef (AR), the investigation of the effect of ARs arrangement on the flow field and how spacing affects the flow field in detail is carried out. For computation, the ARs are characterized by various rows of tube ARs varying their spacing both in longitudinal or transversal direction. The length of the slow flow region is of particular interest. The numerical model is based on a solution of the equations governing momentum and conservation of mass for a incompressible, Newtonian fluid based on Computational Fluid Dynamic (CFD).

MATERIALS AND METHODS

Governing equations: The water flow in the simulation is assumed to consist of an incompressible and viscous Newtonian fluid with a constant density. The flow is in an unsteady state and without heat exchanges. The velocity calculations of water flow are based on the continuity equation. The three-dimensional Reynolds-Average Navier-Stokes (RANS) equation is employed as the momentum equation. The equations are listed as follows:

The momentum equation:

$$\frac{\partial}{\partial t}(\rho u_i) + \frac{\partial}{\partial x_i}(\rho u_i u_i) = -\frac{\partial p}{\partial x_i} + \frac{\partial}{\partial x_j} \left[\mu \frac{\partial u_i}{\partial x_j} - \overline{\rho u_i' u_j'} \right] + S_i \quad (1)$$

The continuity equation:

$$\frac{\partial \rho}{\partial t} + \frac{\partial}{\partial x_i}(\rho u_i) = 0 \quad (2)$$

In Eq. 1 and 2 is the density of the fluid; u_i and u_j are the average velocity components for x, y, z; ρ is the static hydrodynamic pressure; μ is the viscosity; u_i' and u_j' are the fluctuation velocities; $-\overline{\rho u_i' u_j'}$ is the Reynolds stress; i, j = 1, 2, 3 (x, y, z) and S_i is the source item.

In the present study, the Boussinesq hypothesis is assumed to establish the relationships between Reynolds stresses and mean velocity gradients. The equation of Reynolds stresses is given by Eq. 3:

$$\overline{\rho u_i' u_j'} = \mu_t \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) - \frac{2}{3} \left(\rho k + \mu_t \frac{\partial u_i}{\partial x_i} \right) \delta_{ij} \quad (3)$$

Where:

μ_t = The turbulent viscosity

k = The turbulent kinetic energy

Turbulence model: In the present research, the Renormalisation Group (RNG) k- ϵ turbulence model is adopted. This is an improved version of the k- ϵ turbulence model. The new turbulent equations for “k” and “ ϵ ” are listed as follows:

k equation:

$$\frac{\partial(\rho k)}{\partial t} + \frac{\partial(\rho k u_i)}{\partial x_i} = \frac{\partial}{\partial x_j} \left[a_k \mu_{eff} \frac{\partial k}{\partial x_j} \right] + G_k + \rho \epsilon \quad (4)$$

ϵ equation:

$$\frac{\partial(\rho \epsilon)}{\partial t} + \frac{\partial(\rho \epsilon u_i)}{\partial x_i} = \frac{\partial}{\partial x_j} \left[a_k \mu_{eff} \frac{\partial \epsilon}{\partial x_j} \right] + C_{1\epsilon}^* \frac{\epsilon}{k} G_k - C_{2\epsilon}^* \rho \frac{\epsilon^2}{k} \quad (5)$$

In Eq. 4 and 5, G_k is expressed by the average flow gradient based on the turbulent kinetic energy, μ_{eff} is the validity turbulent viscosity coefficient, a_k and a_ϵ inverse turbulent Prandtl numbers for the k and ϵ equations and $C_{1\epsilon}$ and $C_{2\epsilon}$ are known constants. The calculated equations of these items and coefficients are expressed as:

$$G_k = \mu_t \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \frac{\partial u_i}{\partial x_j}, \mu_{eff} = \mu + \mu_t, \\ \mu_t = \rho C_\mu \frac{k^2}{\epsilon}, C_\mu = 0.0845$$

$$a_k = a_e = 1.390, C_{1e}^* = C_{1e} - \frac{\eta(1-\eta/\eta_0)}{1+\beta\eta^3}, C_{1e} = 1.42, C_{2e} = 1.68 \quad (6)$$

$$\eta_0 = 4.377, \beta = 0.012, \eta =$$

$$(2E_{ij} \times E_{ij})^{1/2} \frac{k}{e}, E_{ij} = \frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)$$

Where:

η = A dimensionless parameter

η_0, C_μ = Constants

and β

E_{ij} = The main rate of the strain tensor

CFD Model and boundary conditions: In this study, the computational domain representing the beach area containing the schematic of Artificial Reefs (AR) is shown in Fig. 1. Whilst, the parameters used are defined in detail in Table 1. It should be noted that all of the variables in Table 1 is defined in D in which D is the diameter of artificial reef unit. The domain consists of three rows of artificial reef parallelly deployed at certain distance from the beach line. In the present study, the number of AR row is varied (in this case 1-3 rows). For all following computations in each row 5 AR units are implemented. It should be noted that the value of the width of the domain (L_p) depends on the spacing between AR units in transversal direction (A_c) as shown in Fig. 2. In the present study, the R_c and A_c as shown in Fig. 2 are varied with respect to the velocity distribution surrounding reefs. In this way, the optimal formation of ARs can be obtained. This variation is performed to obtain the most effective formation of AR dealing with the slow flow region. The CFD analysis is performed using ANSYS Fluent 7. The corresponding boundary condition as well as the operational condition for the case studied, here is shown in Fig. 3 and Table 2, respectively.

Numerical method: The generation of the computational grid is performed using ANSYS. In order to discretize the three-dimensional unsteady incompressible Navier-Stokes equation, the finite volume method is applied. A three-dimensional pressure-based solver in a first order implicit steady formulation is adopted. Simple C algorithm is used to solve the pressure and velocity coupling. For the convection terms for momentum, turbulent kinetic energy and turbulent energy dissipation rate equations, a second order upwind discretization scheme is used.

Table 1: The size of computational domain in D (D = Diameter of the artificial reef unit)

Variables	Size
Length of domain (P_p)	115 D
Distance between the reference line and shore line (S_c)	100 D
Depth of domain in inlet section (T_p)	5 D
Height of AR unit (T_c)	3 D
Angle of the bottom, (θ)	2.7°

Table 2: Parameter data used in this simulation

Physical parameters	Values
Velocity of sea water (at inlet, left, right and top section)	1 (m/sec)
Operating pressure	101.325 (Pa)
Density of sea water	1.025 (kg/m ³)
Viscosity of sea water	0.001003 (kg/msec)

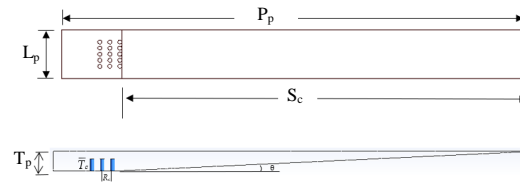


Fig. 1: Schematic of the computational domain containing 3 rows of artificial reefs with parallel formation in horizontal and vertical view (Note: P_p is length of domain, S_c is distance between the reference line and shore line, T_p is depth of domain in inlet section, T_c is height of AR unit, R_c is the spacing between AR units in longitudinal direction and θ is angle of the bottom)

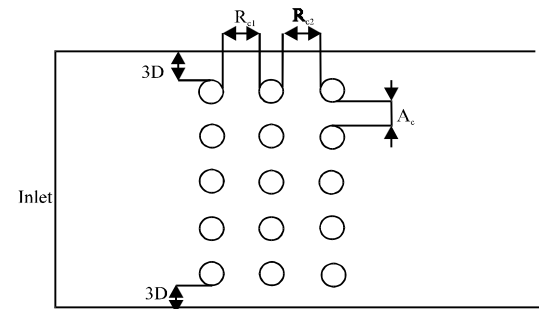


Fig. 2: Artificial reef with 3 rows with parallel formation in horizontal view

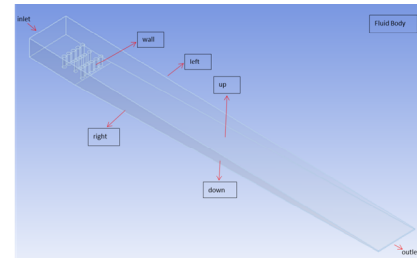


Fig. 3: Boundary conditions of CFD Model in isometric view

RESULTS AND DISCUSSION

In the present study, the flow fields represented by velocity profile for various artificial reef arrangements are analyzed by CFD analysis. The effect of the streamwise and parallel spacing between AR units on the flow fields are explored in detail. The artificial reef arrangements considered here is the tube artificial reef with parallel formation varying number of rows and spacing between AR units as discussed as follows.

Effect of spacing: In order to obtain the behavior of sea water flow within and surrounding the artificial reefs, the first investigation is performed dealing with the absence of the artificial reef. Figure 4 shows the velocity profile along the computational domain of the beach area without artificial reef. It is clear that there is no flow behavior identified in this contour. As mentioned in Table 2, the inlet velocity is 1 m/sec and therefore, based on Fig. 4, it can be seen that most of local velocities shown in the computational domain refers to the velocity values which are the same with the inlet velocity. As a note, when no barrier of flow current is found, the flow back velocity from the shore line will carry the sand and thus, the abrasion occurs. Therefore, it is believed that to reduce the abrasion, the back velocity must be minimized by introducing and deploying the artificial reefs in best arrangement and in right position relatively to the shore line. As is known in nature the existence of the reef can alter the flow characteristic compared to the condition without the reef. Therefore, it is necessary to deploy the artificial reef, so as it can mimic the reef characteristic.

The main goal of this research is to investigate the optimal arrangement of artificial reef varying spacing between AR units and also to determine the right position of the deployment of such artificial reef relatively to the shore line. Thus, the optimal length of the slow flow region is of particular interest. Table 3-5 show the comparison of the velocity profile within and surrounding reefs for various arrangements of artificial reef both in vertical and horizontal view. As is shown in Fig. 2, the arrangement of AR is varied by varying spacing between AR units both in longitudinal (R_c) and transversal (A_c) direction.

Based on Table 3, there are some specific features dealing with the length of slow flow region L_{sf} for the case of Artificial Reef (AR) formation with 1 row. Firstly, in certain condition (in this case when the A_c is decreased by two times, i.e., from $A_c = 1D$ to $A_c = 0.5D$), it seems that



Fig. 4: Velocity profile of the domain without the artificial reef

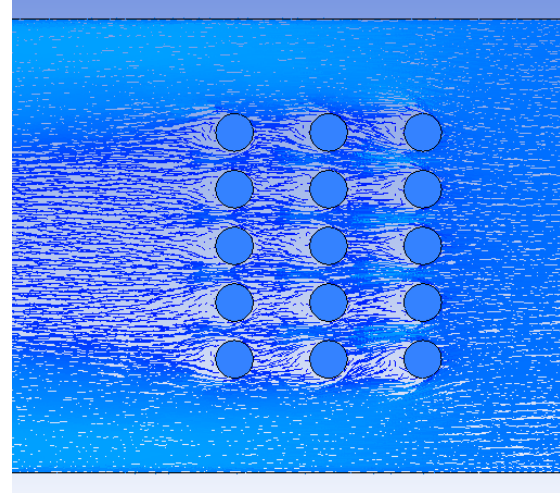


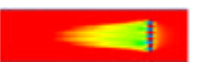


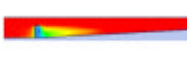






Fig. 5: Velocity vector in horizontal view for the case of optimal AR arrangement with 3 rows

Table 3: Contour of velocity profile for case of AR arrangement with 1 row

Spacing (D)			Horizontal view	Vertical view
A_c	R_{c1}	R_{c2}		
0.5	-	-		
1	-	-		
1.5	-	-		
2	-	-		

increasing the spacing between AR units (A_c in this case) decreases the length of the slow flow region. The decrease in the length of slow flow region is reduced up to 33% when the A_c is reduced up to 100%. However, for another specific feature, it is found that when the A_c is increased from 1-1.5 D, there is no decrease in the length of the slow flow region very much. The difference between the flow characteristic between the case of $A_c = 1D$ and the case of $A_c = 1.5D$ lies in the width of the slow flow region. It can be observed that the width of the slow flow region becomes smaller when the A_c is increased. However, for the case of $A_c = 1.5$ and the case of $A_c = 2$,

Table 4: Contour of velocity profile for case of AR arrangement with 2 rows

Spacing (D)			Horizontal view	Vertical view
A_c	R_{c1}	R_{c2}		
0.5	0.5	-		
0.5	1	-		
0.5	1.5	-		
0.5	2	-		

Table 5: Contour of velocity profile for case of AR arrangement with 3 rows

Spacing (D)			Horizontal view	Vertical view
A_c	R_{c1}	R_{c2}		
0.5	0.5	0.5		
0.5	1	1		
0.5	2	2		
0.5	3	3		

the velocity contour is very similar dealing with the length of the slow flow region as well as the width of the slow flow region. Secondly, increasing the A_c to 1 D makes the slow flow region unique for each AR unit in each row. Based on the ecology point of view, this results in smaller fish zone compared to the AR with $A_c = 1$ D. Based on the hydrodynamic point of view, it seems that for preventing the beach abrasion in the case of artificial reef with 1 row, it is suggested to apply the spacing between AR units, A_c of 0.5 D due to the longest slow flow region. It is also suggested to deploy such artificial reef formation, so as the distance between the ARs and the shore line is 3 m as is shown in detail in Table 3. It should be noted that increased length of slow flow region will attract more fishes and thus enhanced bio-ecosystems.

In the case of AR with 1 row in real application dealing with the main function of artificial reef, it is likely impossible to deploy the AR with the distance of 3 m from the shore line. This is because the fact that bio-ecosystem as well as fish cannot live under circumstance in which the flow behavior is not suitable for them. The water temperature near the shore line is also known hotter so much than the other area. Therefore, it is necessary to add more row on the artificial reef with respect to the length of slow flow region.

Table 4 depicts the contour of velocity profile for the case of artificial reef with 2 rows in parallel formation. The computations are performed by varying the R_c value (in this case, 0.5-2 D with increment of 0.5). It should be noted that for following computations in the case of AR with 2 rows, it is set that the spacing between AR units in longitudinal direction (A_c) is 0.5 D based on the numerical result as shown in Table 3. From Table 4, it can be observed that the length of the slow flow region L_{SF} is strongly affected by the spacing between AR units. The longest L_{SF} of 6 m is obtained when the R_c is 0.5 D. When R_c is increased by factor 2, that is from $R_c = 0.5$ D to $R_c = 1$ D, the L_{SF} reduces by 33%. However, further increasing the R_c does not affect the length of slow flow region. It seems that the trend of flow characteristic in the case of AR with 2 rows is similar to the case of AR with 1 row. There is an optimal spacing in which when this value is increased, the wanted parameter, i.e., slow flow region is not affected by the change of spacing. In comparison to the case of AR with 1 row an interesting thing to note is that for AR with 2 rows, the length of slow flow region is larger (up to 100%). It indicates that the AR with 2 rows is more promising to apply compared to that with 1 row.

With the same frame of the case of artificial reef with 2 rows, Table 5 reflects the comparison of slow flow regions for several arrangements with different R_c values for the case of AR with 3 rows. In the present study, it is assumed that the same spacing is applied on the 2nd and 3rd row of AR units. On the other word, R_{c1} value will be equal to R_{c2} value (Fig. 2). Unlike the case of AR with 2 rows, increasing the R_c does not affect the contour of velocity profile as well as the length of the slow flow region very much. The generated slow flow refers one bigger zone that connects each AR unit. From the ecological and hydrodynamic terms, this generates a best condition for fish and bio-ecosystem. Regarding with the length of the slow flow region, the AR formation with different R_c values predicts the same value, that is 6 m. For beach abrasion prevention, this is the wanted condition. The long L_{SF} makes the deployment of AR possible to apply in real. The back velocity from the shore will reduce if the AR is deployed in right location, so as the sea water does not carry the sand to the middle of the sea.

Based on Table 3-5, it can be concluded that the arrangement and spacing between artificial reef units strongly affect the velocity distribution (i.e., slow flow region) within and surrounding artificial reef. In detail, Table 6 shows the prediction of the length of slow flow region as well as the minimum velocity within the slow flow region for all AR formations. It is found that the artificial reef with 3 rows gives the best flow behavior with respect to the slow flow region, especially, when the formation used is AR with $A_c = 0.5$ $R_{c1} = 0.5$ and $R_{c2} = 0.5$ D. This formation produces the lowest minimum Table

Table 6: Flow characteristics for various artificial reef arrangements and spacings

AR formation/Distance (D)			Velocity (m/sec)	Length of Slow Flow region L_{SF} (m)
Ac	R _{c1}	R _{c2}		
AR with 1 row				
0.5	-	-	0.539	3
1	-	-	0.680	2
1.5	-	-	0.693	1
2	-	-	0.732	1
AR with 2 rows				
0.5	0.5	-	0.473	6
0.5	1	-	0.447	6
0.5	1.5	-	0.420	6
0.5	2	-	0.432	6
0.5	2.5	-	0.582	6
1	0.5	-	0.750	4
1	1	-	0.676	4
1	1.5	-	0.639	4
1	2	-	0.632	4
1.5	0.5	-	0.842	4
1.5	1	-	0.780	4
1.5	1.5	-	0.782	4
1.5	2	-	0.753	4
2	0.5	-	0.862	4
2	1	-	0.858	4
2	1.5	-	0.799	4
2	2	-	0.814	4
AR with 3 rows				
0.5	0.5	0.5	0.458	10
0.5	1	1	0.413	10
0.5	1.5	1.5	0.323	10
0.5	2	2	0.450	10
0.5	2.5	2.5	0.644	10

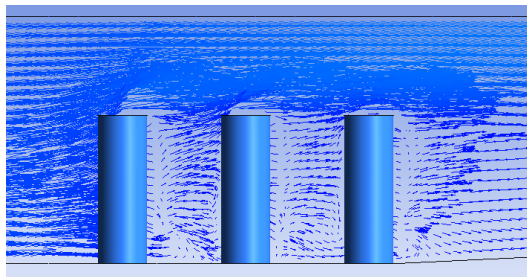


Fig. 6: Velocity vector in vertical view for the case of optimal AR arrangement with 3 rows

velocity of 0.235 m/sec which means that such formation can reduce the velocity up to 76.5% at the farthest distance of 10 m. In his way, the beach abrasion can be reduced significantly.

Velocity vector: Figure 5 shows the velocity vector surrounding reefs with 3 rows in parallel formation which is in this case an optimal AR formation dealing with the length of slow flow region. It can be observed that in around tube reefs, the flow has lower velocities than other region, especially, the flow fields behind the artificial reef. This is expected as the hydrodynamics resulted in surrounding reef produces the back vortex which decelerates the water velocities hitting the reef as seen in

detail in Fig. 6. On the other words, this physical phenomenon leads to the stability of artificial reef structure and it makes the deployment of the artificial reefs more reasonable.

CONCLUSION

In the present study, the three-dimensional turbulent flow within and surrounding tube artificial reef was simulated based on computational fluid dynamic. Different arrangements of artificial reefs varying spacing between AR units both in longitudinal and transversal direction were explored with respect to the length of slow flow region. Some main conclusions are as follows: The closer the spacing between artificial reef units, the longer the length of slow flow region. Increasing the number of row in artificial reef formation enhances the length of slow flow region

The optimal formation of artificial reef with respect to the length of slow flow region is the formation with 3 rows in which $A_c = 0.5$, $R_{c1} = 0.5$ and $R_{c2} = 0.5 D$. It is also suggested to deploy such AR formation at a distance of 10 m behind the last row of AR to reduce the beach abrasion

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REFERENCES

- Bohnsack, J.A. and D.L. Sutherland, 1985. Artificial reef research: A review with recommendations for future priorities. *Bull. Marine Sci.*, 37: 11-39.
- Jiang, Z., Z. Liang, Y. Liu, Y. Tang and L. Huang, 2013. Particle image velocimetry and numerical simulations of the hydrodynamic characteristics of an artificial reef. *Chin. J. Oceanol. Limnol.*, 31: 949-956.
- Jiang, Z., Z. Liang, Y. Tang, L. Huang and D. Yu *et al.*, 2010. Numerical simulation and experimental study of the hydrodynamics of a modeled reef located within a current. *Chin. J. Oceanol. Limnol.*, 28: 267-273.
- Jiao, L., Z. Yan-Xuan, G. Pi-Hai and G. Chang-Tao, 2017. Numerical simulation and PIV experimental study of the effect of flow fields around tube artificial reefs. *Ocean Eng.*, 134: 96-104.

- Kim, D., J. Woo, H.S. Yoon and W.B. Na, 2014. Wake lengths and structural responses of Korean general artificial reefs. *Ocean Eng.*, 92: 83-91.
- Liu, T.L. and D.T. Su, 2013. Numerical analysis of the influence of reef arrangements on artificial reef flow fields. *Ocean Eng.*, 74: 81-89.
- Liu, Y., C.T. Guan, Y.P. Zhao, Y. Cui and G.H. Dong, 2012. Numerical simulation and PIV study of unsteady flow around hollow cube artificial reef with free water surface. *Eng. Appl. Comput. Fluid Mech.*, 6: 527-540.
- Liu, Y., Y.P. Zhao, G.H. Dong, C.T. Guan and Y. Cui *et al.*, 2013. A study of the flow field characteristics around star-shaped artificial reefs. *J. Fluids Struct.*, 39: 27-40.
- Miao, Z.Q. and Y.H. Xie, 2007. Effects of water-depth on hydrodynamic force of artificial reef. *J. Hydrodyn. Ser. B*, 19: 372-377.
- Ontowirjo, B. and H.D. Armono, 2003. Artificial Reef Methodology for Coastal Protection using Submerged Structures: A Numerical Modeling Approach. In: *Soft Shore Protection*, Goudas, C., G. Katsiaris, V. May and T. Karambas (Eds.). Springer, Dordrecht, The Netherlands, ISBN: 978-94-010-3966-6, pp: 211-225.
- Suzuki, G., S. Kai, H. Yamashita, K. Suzuki and Y. Iehisa *et al.*, 2011. Narrower grid structure of artificial reef enhances initial survival of in situ settled coral. *Marine Pollut. Bull.*, 62: 2803-2812.
- Woo, J., D. Kim, H.S. Yoon and W.B. Na, 2014. Characterizing Korean general artificial reefs by drag coefficients. *Ocean Eng.*, 82: 105-114.