ISSN: 1816-949X

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# A Novel Approach for CEED Problem Solution Using AWDO Technique

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Abstract: The current research focuses on the Combined Economic Emission Dispatch (CEED) problem solution for optimal generation of multiple power generating units considering both generation cost and emission satisfying all operational constraints and load demand. The CEED problem reflects the environmental impacts from the gaseous emission of pollutants at fossil-fueled power generating plants. This study presents the formulation of the CEED problem as a multi-objective problem which in turn has been converted into a single objective function considering price penalty factor. A new nature-inspired global optimization method, Adaptive Wind Driven Optimization (AWDO) has been proposed to solve the CEED problem solution. To validate the effectiveness of the proposed algorithm simulation results have been compared with other existing algorithms for two test systems (10 and 40 thermal units) and AWDO has proved to be the best and most powerful amongst them.

**Key words:** Adaptive wind driven optimization, economic load dispatch, constrained minimization, multi objective, valve-point effect, environmental dispatch

## INTRODUCTION

The objective of the Economic Dispatch Problem (EDP) is determining the optimal generation for each generator at minimum fuel costs, conditional on equality constraints on power balance and inequality constraints on power outputs. In addition, transmission losses, higher order non-linear valve point effect may also be considered.

A diversity of techniques has been used by earlier researchers to solve ED (Economic Dispatch) problems of which several are based on classical optimization methods for example, the linear or quadratic programming whereas others are based on artificial intelligence or heuristic algorithms.

During the last two decades, the different conventional techniques such as Lambda-iteration method (Sivanagaraju and Srinivasan, 2010) Gradient method used by Chang *et al.* (2010) and Coleman and Verma (2001) base-point participation factor method (Wood and Wollenberg, 2012) have been applied though the techniques have some limitations. The demerits are high computational time, several local minima and oscillatory in nature (Sahoo *et al.*, 2015).

Contemporary stochastic search algorithms such as PSO used by El-Sawy *et al.* (2013), Vlachogiannis and Lee (2009), Selvakumar and Thanushkodi (2007), Park *et al.* (2010), Sreenivasan *et al.* (2011) and

Shahinzadeh et al. (2014), GA used by Damousis et al. (2003), Walters and Sheble (1993) and Nanda and Narayanan (2002) direct search used by Chen and Chen (2001) and differential evolution used by Balamurugan and Subramanian (2008) and Noman and Iba (2010) simulated annealing used by Vishwakarma et al. (2012) and Basu (2005). Gravitational search used by Mondal et al. (2013) and Hota and Sahu (2015), Cuckoo search used by Tran et al. (2015), Sekhar and Mohanty Binary successive approximation-based evolutionary search used by Dhillon and Kothari (2009) Mallikarjuna et al. have been applied for solving the ELD problem. However, the above mentioned optimization techniques in literature are also accompanying with their own limitations such as local optimal solution and requirement of common controlling parameters like population size, executions of many repeated stages, execution speed etc. Jaya optimization algorithm used by Rao (2016) is a relatively newly developed class of algorithm. Trust-Region reflective algorithm used by Bisheh et al. (2012) is another very effective algorithm that has strong potential to solve constrained optimization problem. This is also a new algorithm. In the present research Wind Driven Optimization (WDO) algorithm has been proposed to solve the CEED problem. It's a global optimization technique that is inspired from nature and its working principle is based on atmospheric motion. The technique is population based heuristic

global optimization algorithm which can be used for multi-dimensional and multi-modal problems. The technique has the ability to implement constrained optimization in search domain.

### MATERIALS AND METHODS

**Problem formulation:** The combined environmental economic dispatch problem is to minimize two objective functions, fuel cost and emission, simultaneously while satisfying all equality and inequality constraints. The mathematical formulation of the problem is described as follows.

## **Economic dispatch formulation with valve point effect:**

The cost function of economic load dispatch problem is defined as follows where  $P_{\scriptscriptstyle G}$  is the total generation:

$$F_{c}(P_{G}) = \sum\nolimits_{i=1}^{Ng} \; \left( a_{i} \; P_{i}^{2} + b_{i} \; P_{i} + c_{i} \right) + \left| d_{i} \; sin\left( e_{i} \; * \left( p_{i}^{\; min} \; - P_{i} \right) \right) \right| \; (1)$$

Where:

N<sub>g</sub> = The number of generating units

 $a_i$ ,  $b_i$ ,  $c_i$ , = The cost coefficients of the ith generating

d<sub>i</sub> and e<sub>i</sub> unit

P<sub>i</sub> = The real power output of the i th generator

**Emission dispatch formulation:** The emission function of economic load dispatch problem is defined as follows:

$$E(P_g) = \sum_{i=1}^{n} 10^{-2} (a_i + \beta_i P_{gi} + \gamma_i P_{gi}^2) + \xi_i \exp(\lambda_i P_{gi})$$
 (2)

where,  $a_i$   $\beta_i$ ,  $\gamma_i$ ,  $\xi_i$  and  $\lambda_i$  are coefficients of the ith generator emission characteristics.

Minimization of fuel cost and emission: The multiobjective combined economic and emission problem with its constraints can be mathematically formulated as a nonlinear constrained problem as follows:

$$OF = \omega \sum\nolimits_{i = 1}^{n} {F(P_{gi})} + (1 \text{-} \omega) \sum\nolimits_{i = 1}^{n} {E(P_{gi})}$$
 (3)

The solution of the problem is achieved by minimizing the Objective Function (OF), the fuel cost rate (\$/h) is shown with F (Pg)and  $NO_x$  emission rate (ton/h) with E (Pg).

**Power balance constraint:** Generation should cover the total demand and the active power losses that occur in the transmission system:

$$\sum_{i=1}^{Ng} j = 1P_i = P_d + P_{loss}$$
 (4)

Where:

 $P_d$  = The total demand load

 $P_{loss}$  = The total transmission losses computed using quadratic approximation

$$P_{loss} = \sum_{i=1}^{Ng} \sum_{i=1}^{Ng} P_i B_{ij} P_j$$
 (5)

where,  $B_{ij}$  is the loss coefficient matrix. This study assumes B-matrix as constant. Power generation limits. Each unit should generate power within its minimum and maximum limits:

$$p_i^{\min} \le p_i \le p_i^{\max} \tag{6}$$

Adaptive wind driven optimization algorithm: The wind driven optimization is a nature inspired population based iterative heuristic global optimization method. One of the important property of this algorithm is Covariance Matrix Adaptive Evolutionary Strategy (CMAES). It means the technique does not need parameters for tuning which is obtained internally without getting input from the user side other than the population size. The algorithm is following the physical equations describing the trajectory of an individual air parcel. The air parcel is influenced of various natural forces in our atmosphere in hydrostatic balance.

Atmospheric motion by the Eulerian description is considered for solving this algorithm. In this Eulerian description it is assumed that air parcel infinitesimally small and its motion follows the Newton's second law of motion. Using Eulerian description, it is possible for computation the velocity and position of the air parcel within the N-dimensional search space.

To achieve the best computational efficiency in an N-dimensional optimization problem some consideration has been taken accordingly. In case of high level of abstraction of wind description, the horizontal movement of air is stronger than the vertical movement, hence, equations are derived accordingly where certain level of simplifications has modified to achieve computational efficiency in an N-dimensional optimization problem. A detailed description of the algorithm and the parameter analysis can be found by Bayraktar *et al.* (2013) and Bayraktar *et al.* (2010). The velocity and the position update rules follow the Eq. 7. The velocity update equation is expressed as:

$$\overrightarrow{u}_{\text{new}} \!=\! (1 \!-\! a) \overrightarrow{u}_{\text{cur}} \!-\! \overrightarrow{g(x_{\text{cur}})} \!+\! \left|1 \!-\! 1/i\right| RT(x_{\text{max}} \!-\! x_{\text{cur}}) \!+\! c \; u_{\text{cur}}^{\text{otehr dim} f(7)}$$

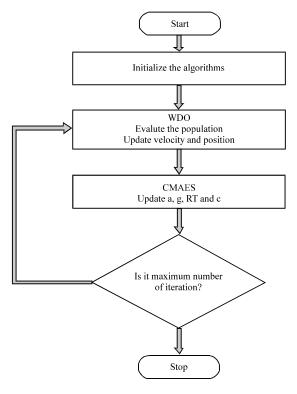


Fig. 1: Flowchart of the adaptive wind driven optimization algorithm

In the expression Eq. 7 presented the rank of the air parcel between all population members based on the pressure value at its location in the search space.

The velocity update equation contains  $\alpha$  which present s the friction coefficient, g that presents the gravitational constant, R which presents the universal gas constant, T that presents the temperature and c which presents a constant that represents the rotation of the Earth.

Initially each parameter is fixed to a constant value. From Eq. 7, it is clearly seen that the updated velocity  $(u_{new})$  can be obtained by using velocity at the current iteration  $(u_{cur})$ , current location of the search space  $(x_{overlap})$ , distance from the highest pressure point  $(x_{max})$  and as well as the velocity at one of the other dimensions (u cur/otherdim). After updating the velocity of the parcel using Eq. 7, consequently the position also is updated by the following Eq. 8:

$$\overrightarrow{\mathbf{x}}_{\text{new}} = \overrightarrow{\mathbf{x}}_{\text{cur}} + \overrightarrow{\mathbf{u}}_{\text{new}} \times \Delta \overrightarrow{\mathbf{t}}$$
 (8)

where  $x_{new}$  indicates the updated position for each air parcel for the next iteration. It is assumed that for all iterative cases unity time step,  $\Delta t = 1$ . The total algorithm has been explained by the flowchart as shown in Fig. 1.

### RESULTS AND DISCUSSION

The practical applicability of AWDO has been applied for two case studies (10 and 40 thermal units) where the objective functions were non smooth due to the valve-point effects.

The AWDO has been applied through coding in MATLAB 7.9.0 (MathWorks, Inc.) and compared with other optimization methods available in literature. All the simulations have been worked out on a 2.2 GHz Intel Pentium processor with 4 GB of RAM.

Case-study 1 for 10 generating systems: This case study has been performed for a test system of 10 thermal units considering the effects of valve-point loading. The relevant data for this system has been shown in Table 1 (Basu, 2011). In the present study, the load demand is P<sub>D</sub> 2000 MW (considering transmission losses). The results for case study-1 applying AWDO are shown in the ELD Solution Table and program, AWDO Algo 10 gen.m has been written in an m-file. Here, the termination criterion has been set as 100 iterations. The m-file has been loaded in the current MATLAB folder. The lower and upper bounds, linear equalities have been set as per the data given in Table 1. From the successive runs the best results were logged and all the best outputs were written in a tabular form (Table 2) for their comparative analysis.

Case-study 2 for 40 generating systems: A case of 40 thermal units was also carried out to check the effectiveness of the present algorithm. The required data is shown in Table 3 (Basu, 2011). The load demand to be satisfied was  $P_D = 10$ , 500MW (without considering transmission losses). To find the optimal generation of power for 40 generating units, the proposed technique has been utilized. The population size, maximum and minimum generation limits and iteration count for the present study has been fixed. The same procedure was followed as in previous case (Fig. 2-5).

The program for AWDO, ELD\_Solution\_AWDO\_Algo\_40\_gen.m has been written in an MATLAB m-file and kept in the current MATLAB directory. The termination criterion has been set as 2000 iterations. Table 4 shows most feasible results for 40 generating units using different methods. The comparative analysis, out of the results in Table 4, puts forth AWDO to be one of the reliable techniques while valve-point effect is considered. To investigate the effectiveness of this approach, it is seeny that in both the two cases the results obtained from AWDO are almost same with the results of

Table 1: Data for the 10 Thermal units (Basu, 2011)

|       | $\mathrm{Pi}^{\mathrm{min}}$ | Pimax |                       |                          | c <sub>1</sub> (\$/MW) <sup>2</sup> |                     | (\$ ei (rad/ | •                     | β <sub>i</sub> (1b/ |  |                       |                              |
|-------|------------------------------|-------|-----------------------|--------------------------|-------------------------------------|---------------------|--------------|-----------------------|---------------------|--|-----------------------|------------------------------|
| Units | (MW)                         | (MW)  | a <sub>1</sub> (\$/h) | b <sub>1</sub> (\$/M Wh) | /h))                                | d <sub>1</sub> (/h) | MW)          | a <sub>i</sub> (1b/h) | MWh)                | γ <sub>i</sub> (1b/(M W) <sup>2</sup> h) | ξ <sub>i</sub> (1b/h) | $\lambda_{\rm i}(1/{ m MW})$ |
| 1     | 10                           | 55    | 1000.403              | 40.5407                  | 0.12951                             | 33                  | 0.0174       | 360.0012              | -3.9864             | 0.04702                                  | 0.25475               | 0.01234                      |
| 2     | 20                           | 80    | 950.606               | 39.5804                  | 0.10908                             | 25                  | 0.0178       | 350.0056              | -3.9524             | 0.04652                                  | 0.25475               | 0.01234                      |
| 3     | 47                           | 120   | 900.705               | 36.5104                  | 0.12511                             | 32                  | 0.0162       | 330.0056              | -3.9023             | 0.04652                                  | 0.25163               | 0.01215                      |
| 4     | 20                           | 130   | 800.705               | 39.5104                  | 0.12111                             | 30                  | 0.0168       | 330.0056              | -3.9023             | 0.04652                                  | 0.25163               | 0.01215                      |
| 5     | 50                           | 160   | 756.799               | 38.5390                  | 0.15247                             | 30                  | 0.0148       | 13.8593               | 0.3277              | 0.00420                                  | 0.24970               | 0.01200                      |
| 6     | 70                           | 240   | 451.325               | 46.1592                  | 0.10587                             | 20                  | 0.0163       | 13.8593               | 0.3277              | 0.00420                                  | 0.24970               | 0.01200                      |
| 7     | 60                           | 300   | 1243.531              | 38.3055                  | 0.03546                             | 20                  | 0.0152       | 40.2669               | -0.5455             | 0.00680                                  | 0.24800               | 0.01290                      |
| 8     | 70                           | 340   | 1049.998              | 40.3965                  | 0.02803                             | 30                  | 0.0128       | 40.2669               | -0.5455             | 0.00680                                  | 0.24990               | 0.01203                      |
| 9     | 135                          | 470   | 1658.569              | 36.3278                  | 0.02111                             | 60                  | 0.0136       | 42.8955               | -0.5112             | 0.00460                                  | 0.25470               | 0.01234                      |
| 10    | 150                          | 470   | 1356.659              | 38.2704                  | 0.01799                             | 40                  | 0.0141       | 42.8955               | -0.5112             | 0.00460                                  | 0.25470               | 0.01234                      |

 $\underline{\text{Table 2: Comparison of best results of different optimization techniques for case study-1, PD} = 2000 \ \underline{\text{MW}}$ 

| -               | MODE (Basu, | PDE (Basu, | NSGA-2       | SPEA         | GSA (Guvenc et al., |           |           |           |
|-----------------|-------------|------------|--------------|--------------|---------------------|-----------|-----------|-----------|
| Units           | 2011)       | 2011)      | (Basu, 2011) | (Basu, 2011) | 2012)               | TLBO      | JOA       | AWDO      |
| P1(MW)          | 54.9487     | 54.9853    | 51.9515      | 52.9761      | 54.9992             | 54.4285   | 55.0000   | 54.9441   |
| P2 (MW)         | 74.5821     | 79.3803    | 67.2584      | 72.8130      | 79.9586             | 78.9558   | 78.4112   | 79.7300   |
| P3 (MW)         | 79.4294     | 83.9842    | 73.6879      | 78.1128      | 79.4341             | 79.5993   | 80.3464   | 80.1338   |
| P4 (MW)         | 80.6875     | 86.5942    | 91.3554      | 83.6088      | 85.0000             | 85.4390   | 84.6690   | 86.2269   |
| P5 (MW)         | 136.8551    | 144.4386   | 134.0522     | 137.2432     | 142.1063            | 143.7134  | 143.8600  | 143.5906  |
| P6 (MW)         | 172.6393    | 165.7756   | 174.9504     | 172.9188     | 166.5670            | 166.9796  | 167.4608  | 165.9426  |
| P7 (MW)         | 283.8233    | 283.2122   | 289.4350     | 287.2023     | 292.8749            | 293.3021  | 292.4104  | 292.7701  |
| P8 (MW)         | 316.3407    | 312.7709   | 314.0556     | 326.4023     | 313.2387            | 312.9163  | 313.2630  | 312.4573  |
| P9 (MW)         | 448.5923    | 440.1135   | 455.6978     | 448.8814     | 441.1775            | 440.4352  | 440.4677  | 440.3041  |
| P10 (MW)        | 436.4287    | 432.6783   | 431.8054     | 423.9025     | 428.6306            | 428.1624  | 428.0384  | 427.8155  |
| Cost (×10^5 \$) | 1.1348      | 1.1351     | 1.1354       | 1.1352       | 1.1349              | 1.1333    | 1.1333    | 1.1330    |
| Emission (lb)   | 4124.9      | 4111.4     | 4130.2       | 4109.1       | 4111.4000           | 4108.1000 | 4105.3000 | 4108.8000 |
| Loss (MW)       | 84.3271     | 83.9331    | 84.2496      | 84.0612      | 83.9869             | 83.9317   | 83.9270   | 83.9150   |

Table 3: Data for the 40 thermal units (Basu, 2011)

Pi<sup>min</sup> Pi<sup>max</sup> h

|       | $\mathbf{Pi}^{\min}$ | $Pi^{max}$ |                       | $\mathbf{b_i}$ | $\mathbf{c}_{\mathrm{i}}$ |                       | ei(rad/ | $\mathbf{a}_{\mathrm{i}}$ | $\beta_i(ton/$ | γ <sub>i</sub> (ton/ |                |                   |
|-------|----------------------|------------|-----------------------|----------------|---------------------------|-----------------------|---------|---------------------------|----------------|----------------------|----------------|-------------------|
| Units | (MW)                 | (MW)       | a <sub>i</sub> (\$/h) | (\$/MWh)       | (\$/MW)2 h)               | d <sub>i</sub> (\$/h) | MW)     | (ton/h)                   | MWh)           | (MW)2h)              | $\xi_i(ton/h)$ | $\lambda_i(1)/MW$ |
| 1     | 36                   | 114        | 94.7050               | 6.730          | 0.00690                   | 100                   | 0.084   | 60                        | -2.22          | 0.0480               | 1.3100         | 0.05690           |
| 2     | 36                   | 114        | 94.7050               | 6.730          | 0.00690                   | 100                   | 0.084   | 60                        | -2.22          | 0.0480               | 1.3100         | 0.05690           |
| 3     | 60                   | 120        | 309.540               | 7.070          | 0.02028                   | 100                   | 0.084   | 100                       | -2.36          | 0.0762               | 1.3100         | 0.05690           |
| 4     | 80                   | 190        | 369.030               | 8.180          | 0.00942                   | 150                   | 0.063   | 120                       | -3.14          | 0.0540               | 0.9142         | 0.04540           |
| 5     | 47                   | 97         | 148.890               | 5.350          | 0.01140                   | 120                   | 0.077   | 50                        | -1.89          | 0.0850               | 0.9936         | 0.04060           |
| 6     | 68                   | 140        | 222.330               | 8.050          | 0.01142                   | 100                   | 0.084   | 80                        | -3.08          | 0.0854               | 1.3100         | 0.05690           |
| 7     | 110                  | 300        | 287.710               | 8.030          | 0.00357                   | 200                   | 0.042   | 100                       | -3.06          | 0.0242               | 0.6550         | 0.02846           |
| 8     | 135                  | 300        | 391.980               | 6.990          | 0.00492                   | 200                   | 0.042   | 130                       | -2.32          | 0.0310               | 0.6550         | 0.02846           |
| 9     | 135                  | 300        | 455.760               | 6.600          | 0.00573                   | 200                   | 0.042   | 150                       | -2.11          | 0.0335               | 0.6550         | 0.02846           |
| 10    | 130                  | 300        | 722.820               | 12.90          | 0.00605                   | 200                   | 0.042   | 280                       | -4.34          | 0.4250               | 0.6550         | 0.02846           |
| 11    | 94                   | 375        | 635.200               | 12.90          | 0.00515                   | 200                   | 0.042   | 220                       | -4.34          | 0.0322               | 0.6550         | 0.02846           |
| 12    | 94                   | 375        | 654.690               | 12.80          | 0.00569                   | 200                   | 0.042   | 225                       | -4.28          | 0.0338               | 0.6550         | 0.02846           |
| 13    | 125                  | 500        | 913.400               | 12.50          | 0.00421                   | 300                   | 0.035   | 300                       | -4.18          | 0.0296               | 0.5035         | 0.02075           |
| 14    | 125                  | 500        | 1760.40               | 8.840          | 0.00752                   | 300                   | 0.035   | 520                       | -3.34          | 0.0512               | 0.5035         | 0.02075           |
| 15    | 125                  | 500        | 1760.40               | 8.840          | 0.00752                   | 300                   | 0.035   | 510                       | -3.55          | 0.0496               | 0.5035         | 0.02075           |
| 16    | 125                  | 500        | 1760.40               | 8.840          | 0.00752                   | 300                   | 0.035   | 510                       | -3.55          | 0.0496               | 0.5035         | 0.02075           |
| 17    | 220                  | 500        | 647.850               | 7.970          | 0.00313                   | 300                   | 0.035   | 220                       | -2.68          | 0.0151               | 0.5035         | 0.02075           |
| 18    | 220                  | 500        | 649.690               | 7.950          | 0.00313                   | 300                   | 0.035   | 222                       | -2.66          | 0.0151               | 0.5035         | 0.02075           |
| 19    | 242                  | 550        | 647.830               | 7.970          | 0.00313                   | 300                   | 0.035   | 220                       | -2.68          | 0.0151               | 0.5035         | 0.02075           |
| 20    | 242                  | 550        | 647.810               | 7.970          | 0.00313                   | 300                   | 0.035   | 220                       | -2.68          | 0.0151               | 0.5035         | 0.02075           |
| 21    | 254                  | 550        | 785.960               | 6.630          | 0.00298                   | 300                   | 0.035   | 290                       | -2.22          | 0.0145               | 0.5035         | 0.02075           |
| 22    | 254                  | 550        | 785.960               | 6.630          | 0.00298                   | 300                   | 0.035   | 285                       | -2.22          | 0.0145               | 0.5035         | 0.02075           |
| 23    | 254                  | 550        | 794.530               | 6.660          | 0.00284                   | 300                   | 0.035   | 295                       | -2.26          | 0.0138               | 0.5035         | 0.02075           |
| 24    | 254                  | 550        | 794.530               | 6.660          | 0.00284                   | 300                   | 0.035   | 295                       | -2.26          | 0.0138               | 0.5035         | 0.02075           |
| 25    | 254                  | 550        | 801.320               | 7.100          | 0.00277                   | 300                   | 0.035   | 310                       | -2.42          | 0.0132               | 0.5035         | 0.02075           |
| 26    | 254                  | 550        | 801.320               | 7.100          | 0.00277                   | 300                   | 0.035   | 310                       | -2.42          | 0.0132               | 0.5035         | 0.02075           |
| 27    | 10                   | 150        | 1055.10               | 3.330          | 0.52124                   | 120                   | 0.077   | 360                       | -1.11          | 1.8420               | 0.9936         | 0.04060           |
| 28    | 10                   | 150        | 1055.10               | 3.330          | 0.52124                   | 120                   | 0.077   | 360                       | -1.11          | 1.8420               | 0.9936         | 0.04060           |
| 29    | 10                   | 150        | 1055.10               | 3.330          | 0.52124                   | 120                   | 0.077   | 360                       | -1.11          | 1.8420               | 0.9936         | 0.04060           |
| 30    | 47                   | 97         | 148.890               | 5.350          | 0.0114                    | 120                   | 0.077   | 50                        | -1.89          | 0.0850               | 0.9936         | 0.04060           |
| 31    | 60                   | 190        | 222.920               | 6.430          | 0.0016                    | 150                   | 0.063   | 80                        | -2.08          | 0.0121               | 0.9142         | 0.04540           |
| 32    | 60                   | 190        | 222.92                | 6.43           | 0.00160                   | 150                   | 0.063   | 80                        | -2.08          | 0.0121               | 0.9142         | 0.045400          |
| 33    | 60                   | 190        | 222.92                | 6.43           | 0.00160                   | 150                   | 0.063   | 80                        | -2.08          | 0.0121               | 0.9142         | 0.045400          |
| 34    | 90                   | 200        | 107.87                | 8.95           | 0.00010                   | 200                   | 0.042   | 65                        | -3.48          | 0.0012               | 0.6550         | 0.028460          |

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|------|-----|---------|--|
|      |     | Continu |  |
|      |     |         |  |

|       | $\mathbf{Pi}^{\min}$ | $\mathrm{Pi}^{\mathrm{max}}$ |                       | $\mathbf{b_i}$ | $c_{i}$     | $\mathbf{d}_{\mathrm{i}}$ | e <sub>i</sub> (rad/ | $\mathbf{a}_{\mathrm{i}}$ | β <sub>i</sub> (ton/ | γ <sub>i</sub> (ton/ |                | _                       |
|-------|----------------------|------------------------------|-----------------------|----------------|-------------|---------------------------|----------------------|---------------------------|----------------------|----------------------|----------------|-------------------------|
| Units | (MW)                 | (MW)                         | a <sub>i</sub> (\$/h) | (\$/MWh)       | (\$/MW)2 h) | (\$/h)                    | MW)                  | (ton/h)                   | MWh)                 | (MW)2h)              | $\xi_i(ton/h)$ | $\lambda_{\rm i}(1)/MW$ |
| 35    | 90                   | 200                          | 116.58                | 8.62           | 0.00010     | 200                       | 0.042                | 70                        | -3.24                | 0.0012               | 0.6550         | 0.02846                 |
| 36    | 90                   | 200                          | 116.58                | 8.62           | 0.00010     | 200                       | 0.042                | 70                        | -3.24                | 0.0012               | 0.6550         | 0.02846                 |
| 37    | 25                   | 110                          | 307.45                | 5.88           | 0.01610     | 80                        | 0.098                | 100                       | -1.98                | 0.0950               | 1.4200         | 0.067700                |
| 38    | 25                   | 110                          | 307.45                | 5.88           | 0.01610     | 80                        | 0.098                | 100                       | -1.98                | 0.0950               | 1.4200         | 0.067700                |
| 39    | 25                   | 110                          | 307.45                | 5.88           | 0.01610     | 80                        | 0.098                | 100                       | -1.98                | 0.0950               | 1.4200         | 0.067700                |
| 40    | 242                  | 550                          | 647.83                | 7.97           | 0.00313     | 300                       | 0.035                | 220                       | -2.68                | 0.0151               | 0.5035         | 0.020750                |

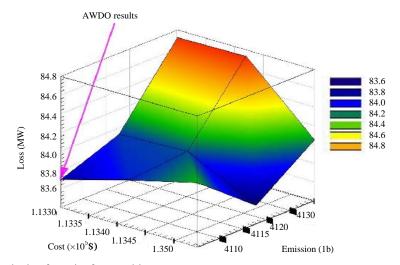


Fig. 2: Comparative analysis of results from Table 2

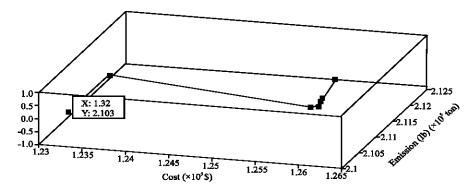


Fig. 3: Comparison of best results of different optimization techniques for case study 2 (from Table 2)

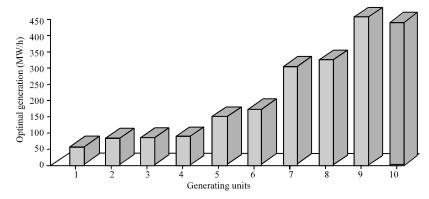


Fig. 4: Optimal generation of case study 1

| Table 4: Con  | parison of best results | of different optimiz | ation techniques for case | study-2, PD = $10,500$ | MW                        |          |          |
|---------------|-------------------------|----------------------|---------------------------|------------------------|---------------------------|----------|----------|
| Units         | MODE (Basu, 2011)       | PDE (Basu, 2011)     | NSGA-2 (Basu, 2011)       | SPEA (Basu, 2011)      | GSA (Guvenc et al., 2012) | TLBO     | AWDO     |
| P1 (MW)       | 113.5295                | 112.1549             | 113.8685                  | 113.9694               | 113.9989                  | 113.9637 | 113.7032 |
| P2 (MW)       | 114                     | 113.9431             | 113.6381                  | 114                    | 113.9896                  | 114.0000 | 114.0000 |
| P3 (MW)       | 120                     | 120                  | 120                       | 119.8719               | 119.9995                  | 119.2759 | 119.9368 |
| P4 (MW)       | 179.8015                | 180.2647             | 180.7887                  | 179.9284               | 179.7857                  | 181.0562 | 180.5315 |
| P5 (MW)       | 96.7716                 | 97                   | 97                        | 97                     | 97                        | 96.4756  | 97.0000  |
| P6 (MW)       | 139.276                 | 140                  | 140                       | 139.2721               | 139.0128                  | 137.7332 | 138.3124 |
| P7 (MW)       | 300                     | 299.8829             | 300                       | 300                    | 299.9885                  | 299.4274 | 300.0000 |
| P8 (MW)       | 298.9193                | 300                  | 299.0084                  | 298.2706               | 300                       | 299.6958 | 300.0000 |
| P9 (MW)       | 290.7737                | 289.8915             | 288.889                   | 290.5228               | 296.2025                  | 298.0269 | 297.1393 |
| P10 (MW)      | 130.9025                | 130.5725             | 131.6132                  | 131.4832               | 130.385                   | 131.0000 | 130.9194 |
| P11 (MW)      | 244.7349                | 244.1003             | 246.5128                  | 244.6704               | 245.4775                  | 245.1809 | 245.2199 |
| P12 (MW)      | 317.8218                | 318.284              | 318.8748                  | 317.2003               | 318.2101                  | 319.6045 | 318.0639 |
| P13 (MW)      | 395.3846                | 394.7833             | 395.7224                  | 394.7357               | 394.6257                  | 394.8243 | 394.2374 |
| P14 (MW)      | 394.4692                | 394.2187             | 394.1369                  | 394.6223               | 395.2016                  | 395.6854 | 396.4756 |
| P15 (MW)      | 305.8104                | 305.9616             | 305.5781                  | 304.7271               | 306.0014                  | 306.6104 | 306.8609 |
| P16 (MW)      | 394.8229                | 394.1321             | 394.6968                  | 394.7289               | 395.1005                  | 393.7669 | 393.9455 |
| P17 (MW)      | 487.9872                | 489.304              | 489.4234                  | 487.9857               | 489.2569                  | 489.3632 | 489.8599 |
| P18 (MW)      | 489.1751                | 489.6419             | 488.2701                  | 488.5321               | 488.7598                  | 489.2599 | 488.5698 |
| P19 (MW)      | 500.5265                | 499.9835             | 500.8                     | 501.1683               | 499.232                   | 499.3462 | 497.9881 |
| P20 (MW)      | 457.0072                | 455.416              | 455.2006                  | 456.4324               | 455.2821                  | 455.8277 | 454.8535 |
| P21 (MW)      | 434.6068                | 435.2845             | 434.6639                  | 434.7887               | 433.452                   | 433.3401 | 432.5556 |
| P22 (MW)      | 434.531                 | 433.7311             | 434.15                    | 434.3937               | 433.8125                  | 432.5457 | 434.2654 |
| P23 (MW)      | 444.6732                | 446.2496             | 445.8385                  | 445.0772               | 445.5136                  | 445.5808 | 444.7076 |
| P24 (MW)      | 452.0332                | 451.8828             | 450.7509                  | 451.897                | 452.0547                  | 453.4598 | 452.8684 |
| P25 (MW)      | 492.7831                | 493.2259             | 491.2745                  | 492.3946               | 492.8864                  | 493.0912 | 492.2676 |
| P26 (MW)      | 436.3347                | 434.7492             | 436.3418                  | 436.9926               | 433.3695                  | 434.2457 | 434.1368 |
| P27 (MW)      | 10                      | 11.8064              | 11.2457                   | 10.7784                | 10.0026                   | 11.2841  | 10.7532  |
| P28 (MW)      | 10.3901                 | 10.7536              | 10                        | 10.2955                | 10.0246                   | 10.6029  | 11.1086  |
| P29 (MW)      | 12.3149                 | 10.3053              | 12.0714                   | 13.7018                | 10.0125                   | 10.9478  | 11.1915  |
| P30 (MW)      | 96.905                  | 97                   | 97                        | 96.2431                | 96.9125                   | 96.2683  | 97.0000  |
| P31 (MW)      | 189.7727                | 190                  | 189.4826                  | 190                    | 189.9689                  | 189.5610 | 189.2526 |
| P32 (MW)      | 174.2324                | 175.3065             | 174.7971                  | 174.2163               | 175                       | 174.3280 | 174.6346 |
| P33 (MW)      | 190                     | 190                  | 189.2845                  | 190                    | 189.0181                  | 188.7028 | 188.8095 |
| P34 (MW)      | 199.6506                | 200                  | 200                       | 200                    | 200                       | 198.2413 | 200.0000 |
| P35 (MW)      | 199.8662                | 200                  | 199.9138                  | 200                    | 200                       | 198.3432 | 198.6563 |
| P36 (MW)      | 200                     | 200                  | 199.5066                  | 200                    | 199.9978                  | 200.2483 | 200.4569 |
| P37 (MW)      | 110                     | 109.9412             | 108.3061                  | 110                    | 109.9969                  | 109.5386 | 109.4282 |
| P38 (MW)      | 109.9454                | 109.8823             | 110                       | 109.6912               | 109.0126                  | 108.7831 | 110.0000 |
| P39 (MW)      | 108.1786                | 108.9686             | 109.7899                  | 108.556                | 109.456                   | 110.0000 | 108.5079 |
| P40 (MW)      | 422.0682                | 421.3778             | 421.5609                  | 421.8521               | 421.9987                  | 420.7631 | 421.7822 |
| Cost (×       | 1.2579                  | 1.2573               | 1.2583                    | 1.2581                 | 1.2578                    | 1.2323   | 1.2322   |
| 10^5 \$)      |                         |                      |                           |                        |                           |          | <b></b>  |
| Emission (lb) | 2.1119                  | 2.1177               | 2.1095                    | 2.111                  | 2.1093                    | 2.114    | 2.103    |
| (21 10 (011)  |                         |                      |                           |                        |                           |          |          |

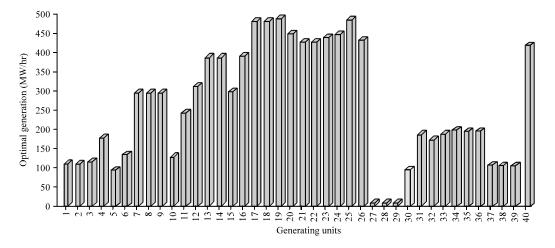


Fig. 5: Optimal generation of case study-2

Box 1: Transmission loss matrix for test system:

|     | 0.000049 | 0.000014 | 0.000015 | 0.000015 | 0.0000160.000017  | 0.000017 | 0.000018 | 0.000019 | 0.000020 |
|-----|----------|----------|----------|----------|-------------------|----------|----------|----------|----------|
|     | 0.000014 | 0.000045 | 0.000016 | 0.000016 | 0.00001700.000015 | 0.000015 | 0.000016 | 0.000018 | 0.000018 |
|     | 0.000015 | 0.000016 | 0.000039 | 0.000010 | 0.000120.000012   | 0.000014 | 0.000014 | 0.000016 | 0.000016 |
|     | 0.000015 | 0.000016 | 0.000010 | 0.000040 | 0.0000140.000010  | 0.000011 | 0.000012 | 0.000014 | 0.000015 |
| B = | 0.000016 | 0.000017 | 0.000012 | 0.000014 | 0.0000350.000011  | 0.000013 | 0.000013 | 0.000015 | 0.000016 |
| Ъ-  | 0.000017 | 0.000015 | 0.000012 | 0.000010 | 0.0000110.000036  | 0.000012 | 0.000012 | 0.000014 | 0.000015 |
|     | 0.000017 | 0.000015 | 0.000014 | 0.000011 | 0.0000130.000012  | 0.000038 | 0.000016 | 0.000016 | 0.000018 |
|     | 0.000018 | 0.000016 | 0.000014 | 0.000012 | 0.0000130.000012  | 0.000016 | 0.000040 | 0.000015 | 0.000016 |
|     | 0.000019 | 0.000018 | 0.000016 | 0.000014 | 0.00001500.000014 | 0.000016 | 0.000015 | 0.000042 | 0.000019 |
|     | 0.000020 | 0.000018 | 0.000016 | 0.000015 | 0.0000160.000015  | 0.000018 | 0.000016 | 0.000019 | 0.000040 |

| Table 5: Standard | deviation | and variance | of case study-1  |
|-------------------|-----------|--------------|------------------|
| Table 5. Standard | ucviation | and variance | or case study -r |

| Algorithms | SD          | Variance  |
|------------|-------------|-----------|
| MODE       | 151.9595040 | 23091.691 |
| PDE        | 147.9068960 | 21876.450 |
| NSGA-2     | 153.3645944 | 23520.699 |
| SPEA       | 151.2236031 | 22868.578 |
| GSA        | 148.6411264 | 22094.184 |
| TLBO       | 148.4512366 | 22037.770 |
| JOA        | 148.3717562 | 22014.178 |
| AWDO       | 148.0821708 | 21928.329 |

Table 6: Standard deviation and variance of case study-2

|            | Table 51 Scaling of Microsit and 1 de lattice 51 sales 5000 / 2 |             |  |  |  |  |  |  |  |
|------------|---|-------------|--|--|--|--|--|--|--|
| Algorithms | SD  | Variance    |  |  |  |  |  |  |  |
| MODE       | 155.6019909   | 24211.97957 |  |  |  |  |  |  |  |
| PDE        | 155.5304779   | 24189.72956 |  |  |  |  |  |  |  |
| NSGA-2     | 155.4116327   | 24152.77559 |  |  |  |  |  |  |  |
| SPEA       | 155.4551195   | 24166.29418 |  |  |  |  |  |  |  |
| GSA        | 155.5556727   | 24197.56731 |  |  |  |  |  |  |  |
| TLBO       | 155.6011394   | 24211.71459 |  |  |  |  |  |  |  |
| AWDO       | 155.4083704   | 24151.7616  |  |  |  |  |  |  |  |

other existing methods. From Table 2 and 4 it is seen that AWDO gives viable results in both the cases. For 10 thermal units (case-study 1), AWDO decreased the fuel cost as well as total transmission loss. The B-matrix for test system-1 is shown in equation transmission loss matrix for test system:

Figure 5 in case study-2 (test system-2) AWDO has worked effectively decreasing both generation cost and emission. Table 5 and 6 show the standard deviation and variance of case study-1 and case study-2, respectively and in both the cases AWDO proved to be effective.

### CONCLUSION

The current research emphases on application of Adaptive Wind Driven Optimization Algorithm (AWDOA) for multi-objective CEED problem solution for examining the performances of two test cases (10 thermal units and 40 thermal units). Satisfactory results are obtained by adapting the program. Simulation results are also compared with other existing algorithms for the above two test cases and AWDO has proved to be the best and most powerful amongst them.

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